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RIGID BODY KINEMATICS

Purpose:

- **Analytical Description of Rigid Body Motion.**
- **Matrix Transforms to Represent Rigid Body Motion.**
- **Reinforcement of Elementary Kinematical Equations.**

Topics:

- **Translation of Rigid Bodies.**
- **Rotation of Rigid Bodies.**
- **General Motion of Rigid Bodies (i.e. Robot Kinematics)**
- **Coordinate Transformations**



Rotation About an Arbitrary Axis (Equivalent Angle-Axis Representation):

Euler's Theorem(10-continued): Any change of orientation for a rigid body with a fixed body point can be accomplished through a *General Rotation Operator* (a simple rotation) with a proper axis and angle selection.

Consider the following coordinates:

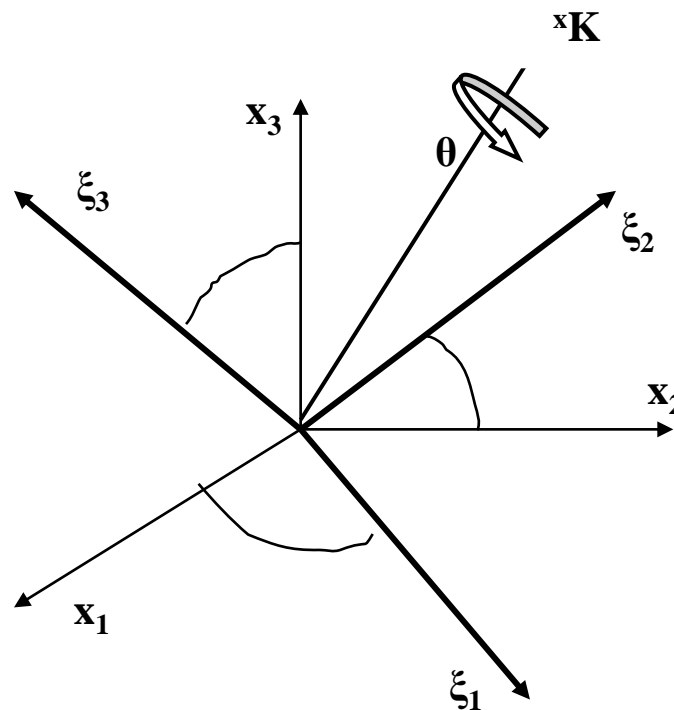
$\{x_i\}$: Spatial Coordinates

$\{\xi_j\}$: Body Coordinates

$$\{x_i\} = \underline{\underline{R}}\{\xi_j\}$$

$$\underline{\underline{R}} = \underline{\underline{R}}({}^x K, \theta) = {}^\xi \underline{\underline{R}}({}^x K, \theta)$$

= A Simple/General Rotation Operator about an arbitrary axis.



Where:

$$\underline{\underline{R}}(^x \underline{K}, \theta) = \begin{bmatrix} k_{x1} k_{x1} v\theta + c\theta & k_{x1} k_{x2} v\theta - k_{x3} s\theta & k_{x1} k_{x3} v\theta + k_{x2} s\theta \\ k_{x1} k_{x2} v\theta + k_{x3} s\theta & k_{x2} k_{x2} v\theta + c\theta & k_{x2} k_{x3} v\theta - k_{x1} s\theta \\ k_{x1} k_{x3} v\theta - k_{x2} s\theta & k_{x2} k_{x3} v\theta + k_{x1} s\theta & k_{x3} k_{x3} v\theta + c\theta \end{bmatrix}$$

And;

$$^x \underline{K} = k_{x1} \underline{e}_1 + k_{x2} \underline{e}_2 + k_{x3} \underline{e}_3 = [k_{x1} \quad k_{x2} \quad k_{x3}]^t \quad \text{and} \quad k_{x1}^2 + k_{x2}^2 + k_{x3}^2 = 1$$

$$v\theta = vers\theta = (1 - \cos\theta)$$

Ex:

$$\underline{\underline{R}}(x_1, \theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & -\sin\theta \\ 0 & \sin\theta & \cos\theta \end{bmatrix} \quad \text{is} \quad \underline{\underline{R}}(^x \underline{K}, \theta) \quad \text{where : } k_{x1} = 1, \quad k_{x2} = 0, \quad k_{x3} = 0$$



For a given Rotation Matrix like

$$\underline{\underline{R}} = {}^x_{\xi} R({}^x K, \theta) = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \text{ one}$$

Can Determine the equivalent angle-axis by taking an inverse approach, such that:

$$\sin \theta = \pm \frac{1}{2} \sqrt{(r_{32} - r_{23})^2 + (r_{13} - r_{31})^2 + (r_{21} - r_{12})^2}, \text{ and}$$

$$\cos \theta = \frac{r_{11} + r_{22} + r_{33} - 1}{2}, \text{ where:}$$



$$\theta = \tan^{-1} \left(\frac{\sin \theta}{\cos \theta} \right)$$

$${}^x K = \frac{1}{2 \sin \theta} \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix} = \begin{bmatrix} k_{x1} \\ k_{x2} \\ k_{x3} \end{bmatrix}$$



This solution is valid for ($0 < \theta < 180$), and for every pair of equivalent angle-axis $(^x \underline{K}, \theta)$, there exists another pair as $(-^x \underline{K}, -\theta)$ representing the same orientation in space with the same rotation matrix. (no solutions for $\theta=0$ and 180).

Any combination of Rotations is always equivalent to a single rotation about some axis “K” by an angle “θ”.

Ex: Let

$$\underline{\underline{R}} = \underline{\underline{R}}(x_2, 90) \underline{\underline{R}}(x_3, 90) = \begin{bmatrix} 0 & 0 & 1 \\ 0 & 1 & 0 \\ -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}$$

From above equations we have:



$$\sin \theta = \pm \sqrt{(1-0)^2 + (1-0)^2 + (1-0)^2} = \pm \frac{\sqrt{3}}{2}$$

$$\cos \theta = \frac{0+0+0-1}{2} = \frac{-1}{2}$$

$$\theta = \tan^{-1}\left(\frac{\pm \sqrt{3}/2}{-1/2}\right) = \pm 120^\circ$$

$$\underline{\underline{K}} = \frac{1}{\sqrt{3}}\underline{e}_1 + \frac{1}{\sqrt{3}}\underline{e}_2 + \frac{1}{\sqrt{3}}\underline{e}_3, \text{ and } -\underline{\underline{K}} = -\left(\frac{1}{\sqrt{3}}\underline{e}_1 + \frac{1}{\sqrt{3}}\underline{e}_2 + \frac{1}{\sqrt{3}}\underline{e}_3\right)$$

$$\underline{\underline{R}} = \underline{\underline{R}}(x_2, 90)\underline{\underline{R}}(x_3, 90) = \underline{\underline{R}}(\underline{\underline{K}}, 120) = \underline{\underline{R}}(-\underline{\underline{K}}, -120)$$



Infinitesimal Rotations, Angular Velocity, and Angular Acceleration:

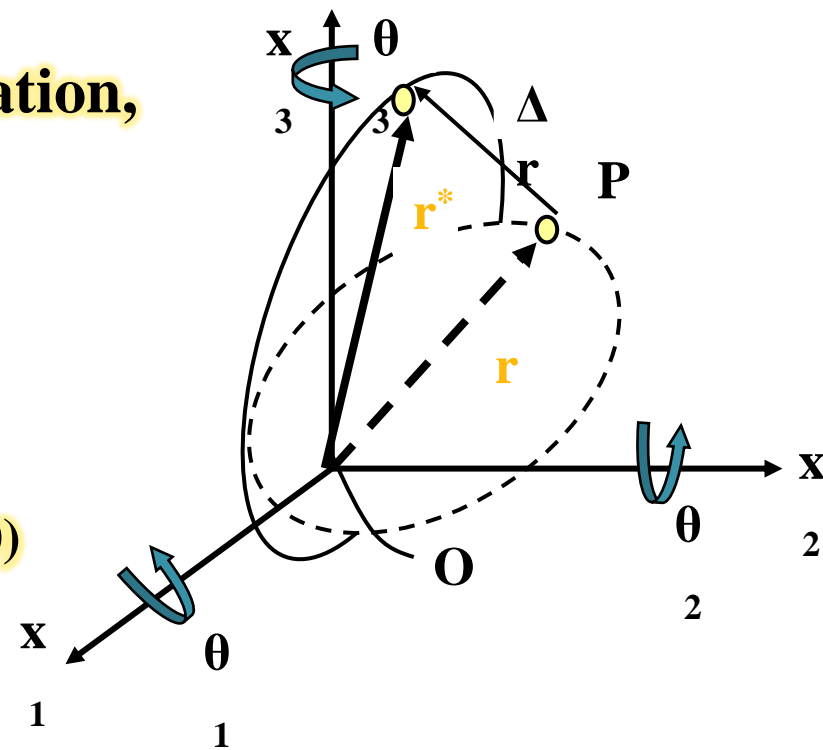
Theorem-11: For general infinitesimal rotations, sequential of the axes of rotation is not important.

Let us consider the displacement of a body point in a rotating rigid body:

\underline{r}^* is the vector \underline{r} after $\underline{\underline{R}}$ Rotation, therefore:

$$\underline{r}^* = \underline{\underline{R}} \underline{r}, \text{ and}$$

$$\Delta \underline{r} = \underline{r}^* - \underline{r} = (\underline{\underline{R}} - \underline{\underline{I}}) \underline{r} \quad (4.10)$$



If we let that \mathbf{x}_1 and \mathbf{x}_3 to be the axes of rotation, we have:

$$\underline{\underline{R}}_1 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\theta_1 & -s\theta_1 \\ 0 & s\theta_1 & c\theta_1 \end{bmatrix}, \quad \text{and} \quad \underline{\underline{R}}_3 = \begin{bmatrix} c\theta_3 & -s\theta_3 & 0 \\ s\theta_3 & c\theta_3 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\underline{\underline{R}}_{13} = \underline{\underline{R}}_1 \underline{\underline{R}}_3 = \begin{bmatrix} c\theta_3 & -s\theta_3 & 0 \\ c\theta_1 s\theta_3 & c\theta_1 c\theta_3 & -s\theta_1 \\ s\theta_1 s\theta_3 & s\theta_1 c\theta_3 & c\theta_1 \end{bmatrix} \quad \& \quad \underline{\underline{R}}_{31} = \underline{\underline{R}}_3 \underline{\underline{R}}_1 = \begin{bmatrix} c\theta_3 & -s\theta_3 c\theta_1 & s\theta_3 s\theta_1 \\ s\theta_3 & c\theta_1 c\theta_3 & -s\theta_1 c\theta_3 \\ 0 & s\theta_1 & c\theta_1 \end{bmatrix}$$

$$\underline{\underline{R}}_{13} \neq \underline{\underline{R}}_{31} \quad (4.11)$$

Now let: $\theta = \Delta\theta = O(\varepsilon) = \text{very - small} \Rightarrow \cos\theta \rightarrow 1, \text{ and } \sin\theta \rightarrow \Delta\theta$
 $O(\varepsilon^2) = 0$




Then:

$$\underline{\underline{R}}_{13} = \begin{bmatrix} 1 & -\Delta\theta_3 & 0 \\ \Delta\theta_3 & 1 & -\Delta\theta_1 \\ 0 & \Delta\theta_1 & 1 \end{bmatrix}, \quad \text{and} \quad \underline{\underline{R}}_{31} = \begin{bmatrix} 1 & -\Delta\theta_3 & 0 \\ \Delta\theta_3 & 1 & -\Delta\theta_1 \\ 0 & \Delta\theta_1 & 1 \end{bmatrix} \Rightarrow$$

$$\underline{\underline{R}}_{13} = \underline{\underline{R}}_{31}$$

Therefore, for General Infinitesimal Rotations we have:

$$\underline{\underline{R}} = \underline{\underline{R}}_1 \underline{\underline{R}}_2 \underline{\underline{R}}_3 = \underline{\underline{R}}_3 \underline{\underline{R}}_2 \underline{\underline{R}}_1 \equiv \begin{bmatrix} 1 & -\Delta\theta_3 & \Delta\theta_2 \\ \Delta\theta_3 & 1 & -\Delta\theta_1 \\ -\Delta\theta_2 & \Delta\theta_1 & 1 \end{bmatrix}, \text{ or } R_{jk} = \delta_{jk} - \gamma_{ijk} \Delta\theta_i$$

(4.12) 

The displacement vect $\Delta \underline{r}$ or due to such combination of rotations will be:

$$\Delta \underline{r} = \underline{r}^* - \underline{r} = (\underline{\underline{R}} - \underline{\underline{I}}) \underline{r} \quad \text{or} \quad \Delta x_i = (R_{ik} - \delta_{ik}) x_k = -\gamma_{jik} \Delta\theta_j x_k = \gamma_{ijk} \Delta\theta_j x_k$$

In matrix form:



$$\Delta \underline{r} = \begin{bmatrix} 0 & -\Delta\theta_3 & \Delta\theta_2 \\ \Delta\theta_3 & 0 & -\Delta\theta_1 \\ -\Delta\theta_2 & \Delta\theta_1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} \quad (4.13)$$

$$\Delta x_i = \gamma_{ijk} \Delta\theta_j x_k \quad \Rightarrow \quad \Delta \underline{r} = \Delta \underline{\theta} \times \underline{r}$$

(from the definition of cross product)

Since \underline{r} is a vector of constant magnitude in the rigid body, we have:

$$\lim_{\Delta t \rightarrow 0} \frac{\Delta \underline{r}}{\Delta t} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \underline{\theta}}{\Delta t} \times \underline{r} \quad \Rightarrow \quad \dot{\underline{r}} = \underline{\omega} \times \underline{r} \quad \text{where;}$$

$$\underline{\omega} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \underline{\theta}}{\Delta t} = \omega_i \underline{e}_i \quad (\text{Angular - Velocity}) \quad (4.14)$$

$$\dot{\underline{r}} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \underline{r}}{\Delta t}$$



Angular Velocity Vector:

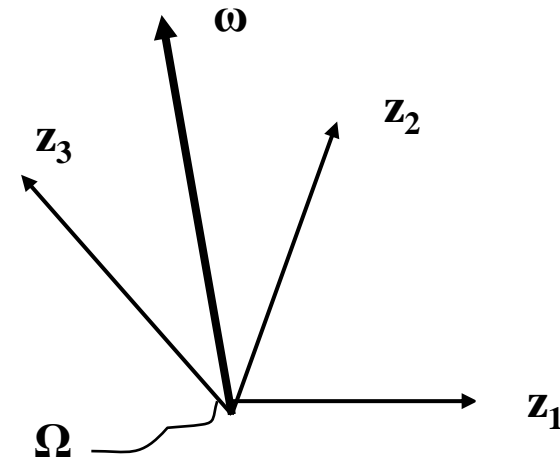
$\underline{\omega} = \omega_i \underline{e}_i$ = (sum of the rotation rates about various axes).

If the angular velocity vector “ $\underline{\omega}$ ” is defined (expressed) in a set of moving coordinates $\{z_i\}$ having an angular velocity “ $\underline{\Omega}$ ”, we may apply the Jaumann rate of a vector to compute the angular acceleration vector.

Angular Acceleration Vector:

$$\underline{\alpha} = \dot{\omega}_i \underline{e}_i + \omega_i \dot{\underline{e}}_i = \dot{\omega}_i \underline{e}_i + \omega_i (\underline{\Omega} \times \underline{e}_i) = \dot{\omega}_i \underline{e}_i + \underline{\Omega} \times \underline{\omega}$$

(4.15)



Note: Even if the rotation rates are constant, there will be an angular acceleration whenever any of the axes do not have a fixed orientation.



Velocity and Acceleration Field in a Rotating Rigid Body:

Consider the rotating rigid body shown:

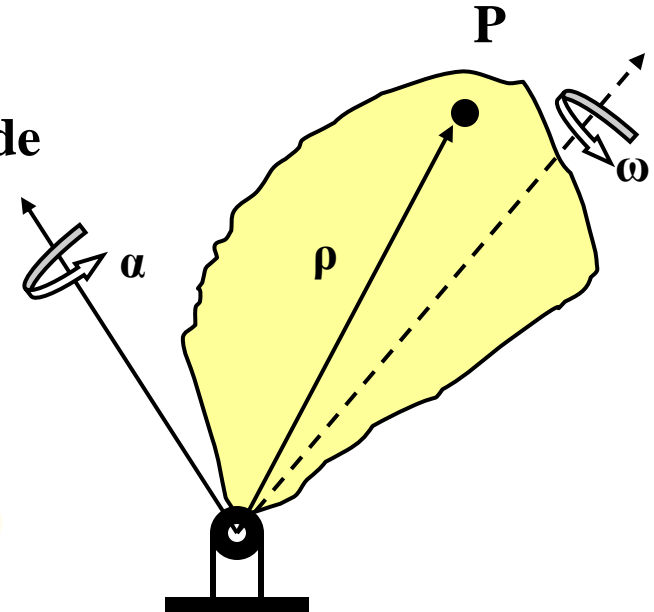
Given: $\underline{\omega}$ and $\underline{\alpha}$ as shown, and
 $\underline{\rho}$: vector of constant magnitude
fixed in the rigid body.

We have:

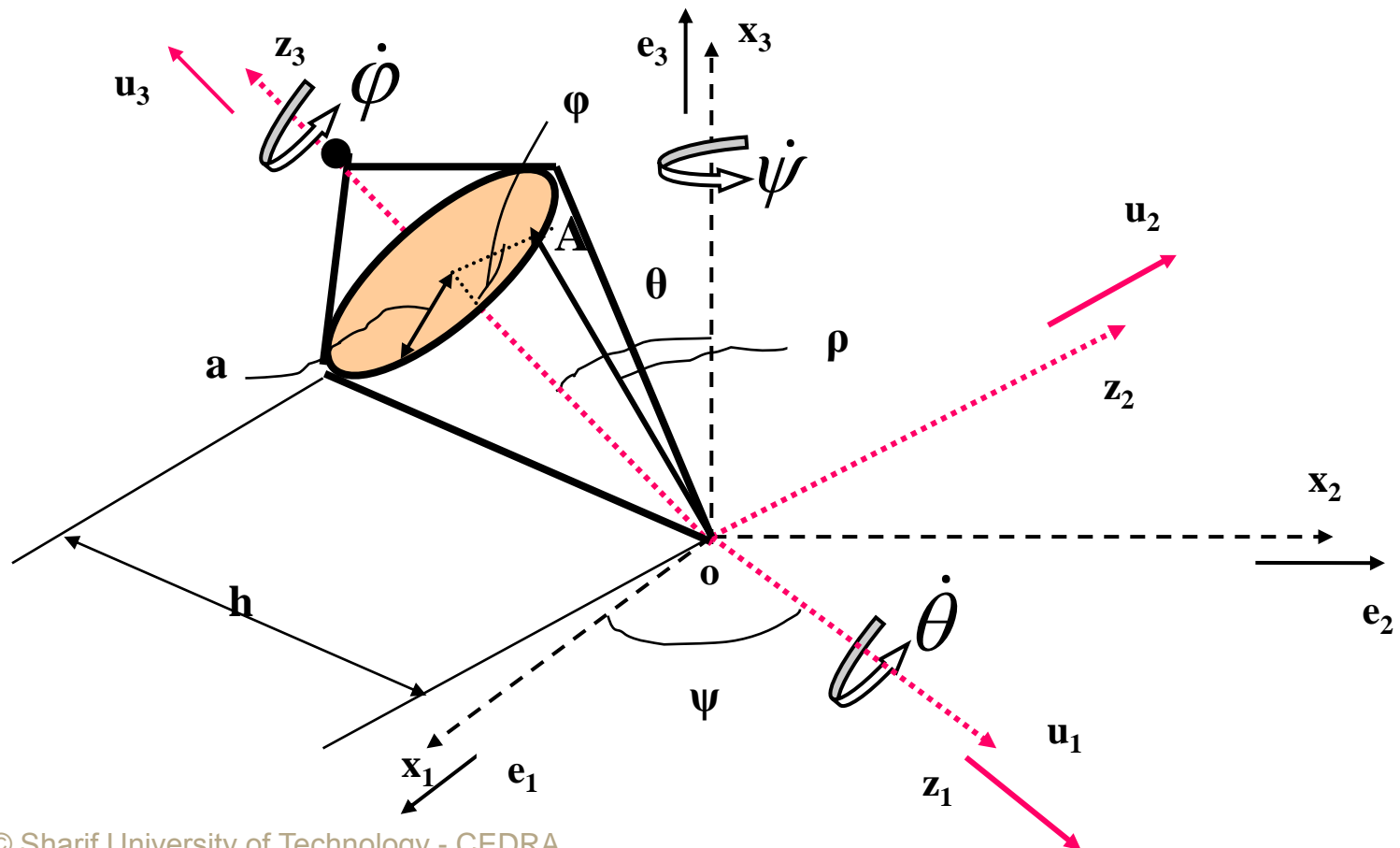
$$\underline{v}_P = \underline{\dot{\rho}} = \underline{\omega} \times \underline{\rho} \quad (4.16)$$

$$\underline{a}_P = \underline{\dot{v}}_P = \underline{\dot{\omega}} \times \underline{\rho} + \underline{\omega} \times \underline{\dot{\rho}} =$$

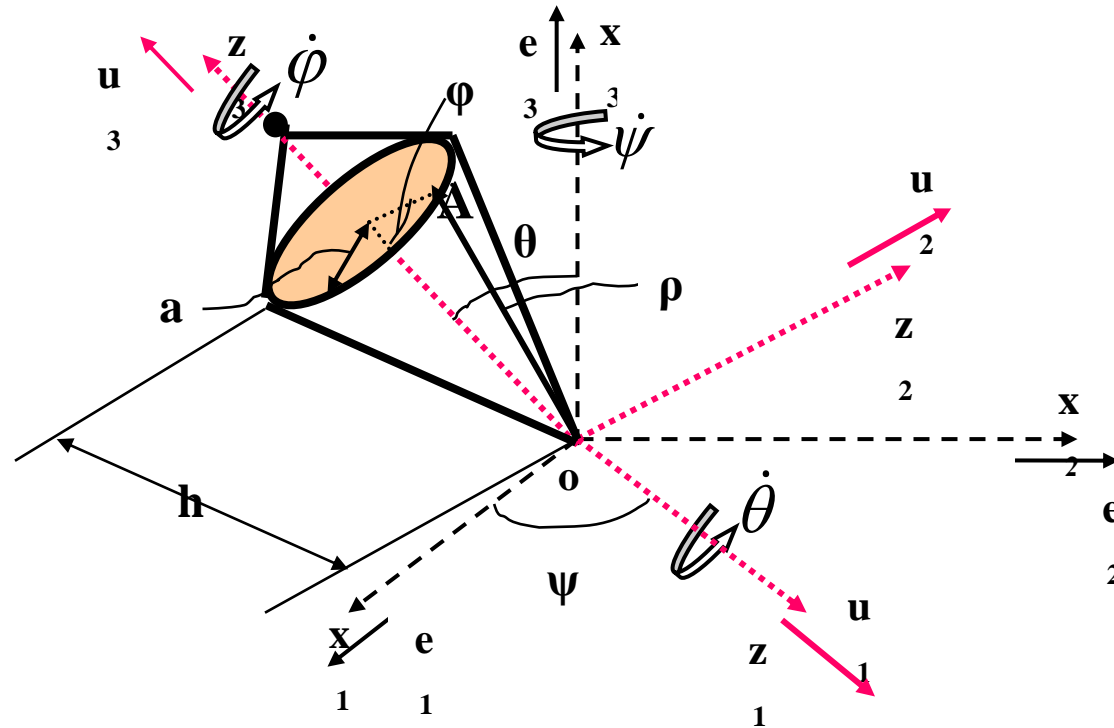
$$\underline{a}_P = \underline{\alpha} \times \underline{\rho} + \underline{\omega} \times (\underline{\omega} \times \underline{\rho}) \quad (4.17)$$



Ex: A top *spins* at a constant speed “ $\dot{\phi}$ ” at a fixed spot “O”. Meanwhile, it *precesses* about the vertical axis at a speed “ $\dot{\psi}$ ”, and its altitude *nutates* at a speed “ $\dot{\theta}$ ” as shown. Determine the velocity and acceleration of a point “A” on its upper rim?

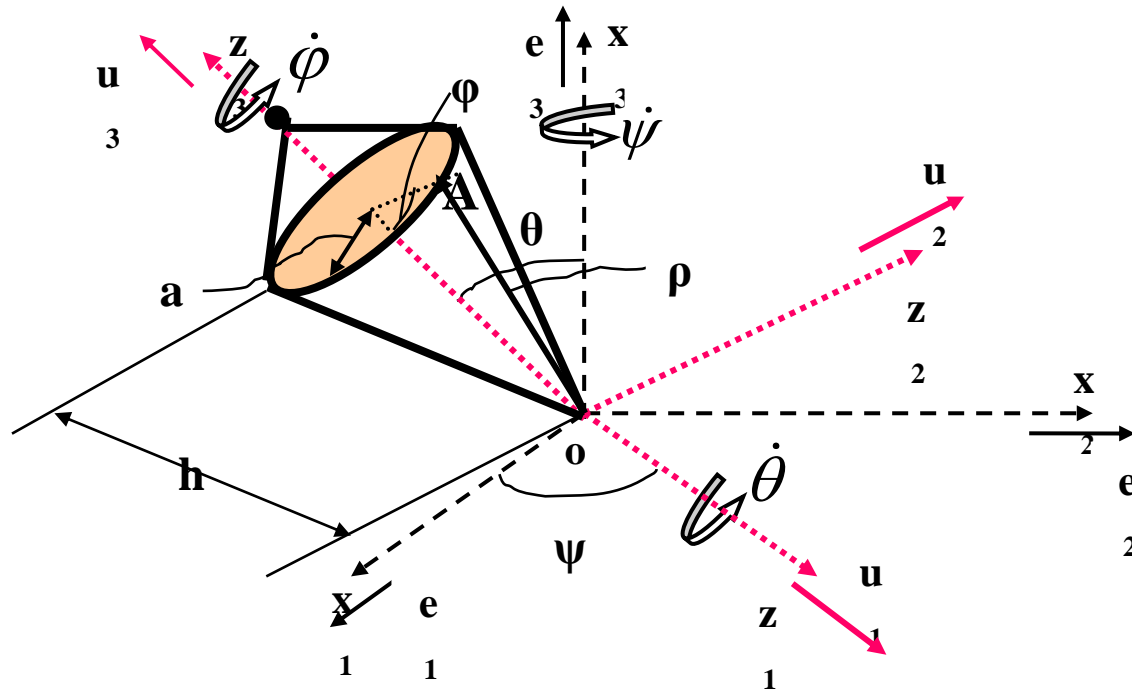


$\{z_j\}$: rotating coordinate in which the top spins only.


$$\underline{\underline{\Omega}} = \dot{\psi} \underline{e}_3 + \dot{\theta} \underline{u}_1$$

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Angular Velocity of $\{z_j\}$:

$$\underline{\underline{\Omega}} = \dot{\psi} \underline{e}_3 + \dot{\theta} \underline{u}_1$$

Angular Velocity of the top: $\underline{\underline{\omega}} = \underline{\underline{\Omega}} + \dot{\phi} \underline{u}_3 = \dot{\psi} \underline{e}_3 + \dot{\theta} \underline{u}_1 + \dot{\phi} \underline{u}_3$

In terms of the rotating coordinate $\{z_j\}$:

$$\underline{\underline{\Omega}} = \dot{\theta} \underline{u}_1 + \dot{\psi} \sin \theta \underline{u}_2 + \dot{\psi} \cos \theta \underline{u}_3$$

$$\underline{\underline{\omega}} = \dot{\theta} \underline{u}_1 + \dot{\psi} \sin \theta \underline{u}_2 + (\dot{\phi} + \dot{\psi} \cos \theta) \underline{u}_3$$



Angular Acceleration of the top: Note that $\underline{\omega}$ is expressed in a set of moving coordinate $\{\underline{z}_j\}$, to find $\underline{\alpha}$ use the **Jaumann** rate of a vector as:

$$\begin{aligned}\underline{\alpha} &= \dot{\omega}_i \underline{e}_i + \underline{\Omega} \times \underline{\omega} = \ddot{\theta} \underline{u}_1 + (\ddot{\psi} \sin \theta + \dot{\psi} \dot{\theta} \cos \theta) \underline{u}_2 + (\ddot{\psi} \cos \theta - \dot{\psi} \dot{\theta} \sin \theta) \underline{u}_3 + \\ &\quad (\dot{\theta} \underline{u}_1 + \dot{\psi} \sin \theta \underline{u}_2 + \dot{\psi} \cos \theta \underline{u}_3) \times [\dot{\theta} \underline{u}_1 + \dot{\psi} \sin \theta \underline{u}_2 + (\dot{\phi} + \dot{\psi} \cos \theta) \underline{u}_3] = \\ \underline{\alpha} &= (\ddot{\theta} + \dot{\phi} \dot{\psi} \sin \theta) \underline{u}_1 + (\ddot{\psi} \sin \theta + \dot{\psi} \dot{\theta} \cos \theta - \dot{\phi} \dot{\theta}) \underline{u}_2 + (\ddot{\psi} \cos \theta - \dot{\psi} \dot{\theta} \sin \theta) \underline{u}_3\end{aligned}$$



Step-2: Absolute Motion Analysis

Position Vector of A in $\{\underline{z}_j\}$:

$$\underline{\rho} = a \cos \varphi \underline{u}_1 + a \sin \varphi \underline{u}_2 + h \underline{u}_3$$

Velocity Vector:

$$\underline{v}_A = \underline{\omega} \times \underline{\rho}$$

Acceleration Vector:

$$\underline{a}_A = \underline{\alpha} \times \underline{\rho} + \underline{\omega} \times (\underline{\omega} \times \underline{\rho})$$



For example if $\dot{\varphi} = 1000 \text{ rpm} = \text{constant} \Rightarrow \varphi = 1000\left(\frac{2\pi}{60}\right)t \text{ rad}$,

$\theta = 0.2\sin(100\pi t) \text{ rad}$, and $\psi = 0.5\sin(50\pi t) \text{ rad}$, then for a specific

time (i.e. 2 ms) one can convert the results presented in rotating

coordinate- $\{z_j\}$, to the space-fixed coordinate- $\{x_i\}$, using the rotation

transformation “ $\underline{\underline{R}} = \underline{\underline{R}}_{\psi} \underline{\underline{R}}_{\theta} \underline{\underline{R}}_{\varphi}$ ” between the two coordinates as:

$$\{\underline{\rho}\}_x = \underline{\underline{R}}\{\underline{\rho}\}_z, \quad \{\underline{v}_A\}_x = \underline{\underline{R}}\{\underline{v}_A\}_z, \quad \{\underline{a}_A\}_x = \underline{\underline{R}}\{\underline{a}_A\}_z, \quad \{\underline{\omega}\}_x = \underline{\underline{R}}\{\underline{\omega}\}_z, \quad \{\underline{\alpha}\}_x = \underline{\underline{R}}\{\underline{\alpha}\}_z$$



General Motion of a Rigid Body (Translation & Rotation):

Chasle's Theorem(12): The general motion of a rigid body can be described by a combination of motion of some convenient reference body point and an Eulerian rotation about that point.

Note: A rigid body in space possesses Six-Degrees-of-Freedom:

3-DOF: for the position of the reference point (rigid body), and

3-DOF: for the orientation of the rigid body (i.e. Euler's Angles).

Let us consider the motion of a moving rigid body in space:



Let us consider the motion of a moving rigid body in space:

$$\underline{\omega} = \omega_i \underline{e}_i, \text{ and } \underline{\alpha} = \alpha_i \underline{e}_i$$

Suppose that the motion of a body point “O” in the rigid body is known, and we wish to compute the motion of another body point “P”?

Position Vector:

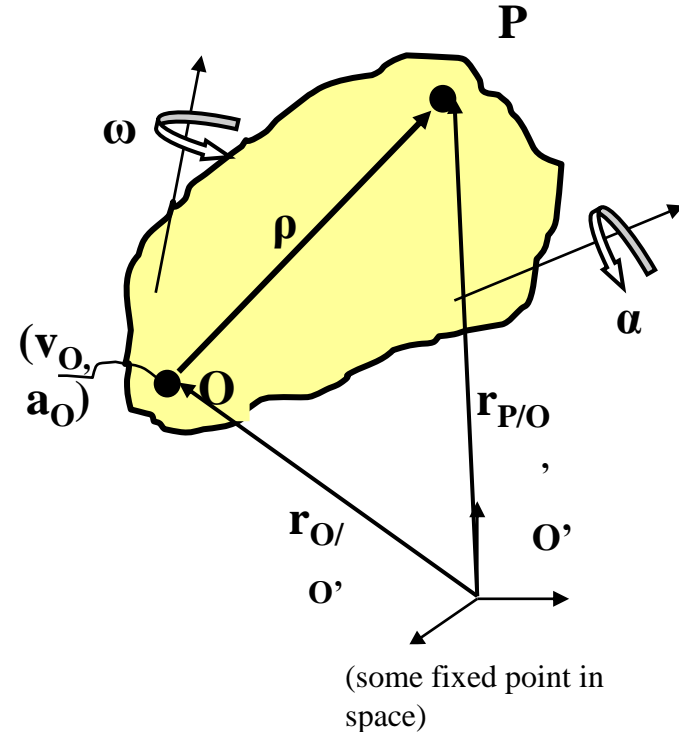
$$\underline{r}_{P/O'} = \underline{r}_{O/O'} + \underline{\rho} \quad (4.18)$$

Velocity Vector:

$$\underline{v}_P = \frac{d\underline{r}_{P/O'}}{dt} = \dot{\underline{r}}_{O/O'} + \dot{\underline{\rho}} = \underline{v}_O + \underline{\omega} \times \underline{\rho} \quad (4.19)$$

Acceleration Vector:

$$\underline{a}_P = \underline{a}_O + \underline{\alpha} \times \underline{\rho} + \underline{\omega} \times (\underline{\omega} \times \underline{\rho}) \quad (4.20)$$



Ex: Given the velocity and acceleration of the block “A” in a double slide mechanism shown. Determine the velocity and acceleration of the block “B”? The hinges at A and B are both of the **ball-and-socket** type.

Given: \underline{v}_A and \underline{a}_A ,

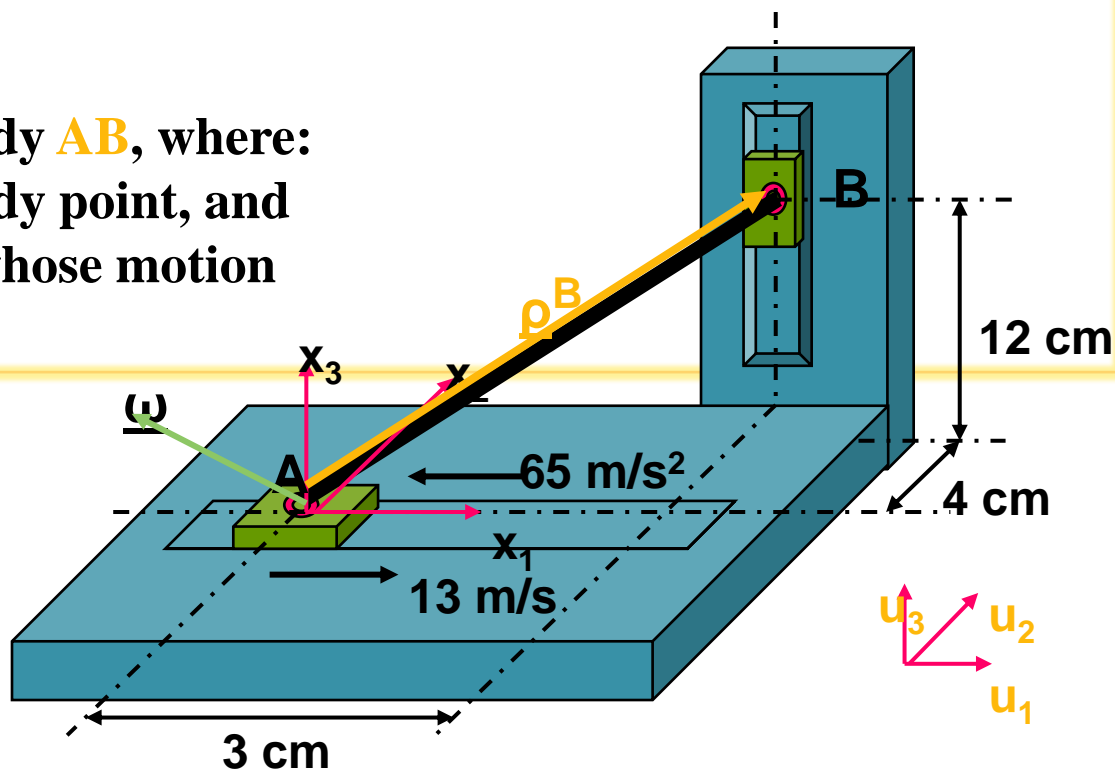
Find: \underline{v}_B and $\underline{a}_B = ?$

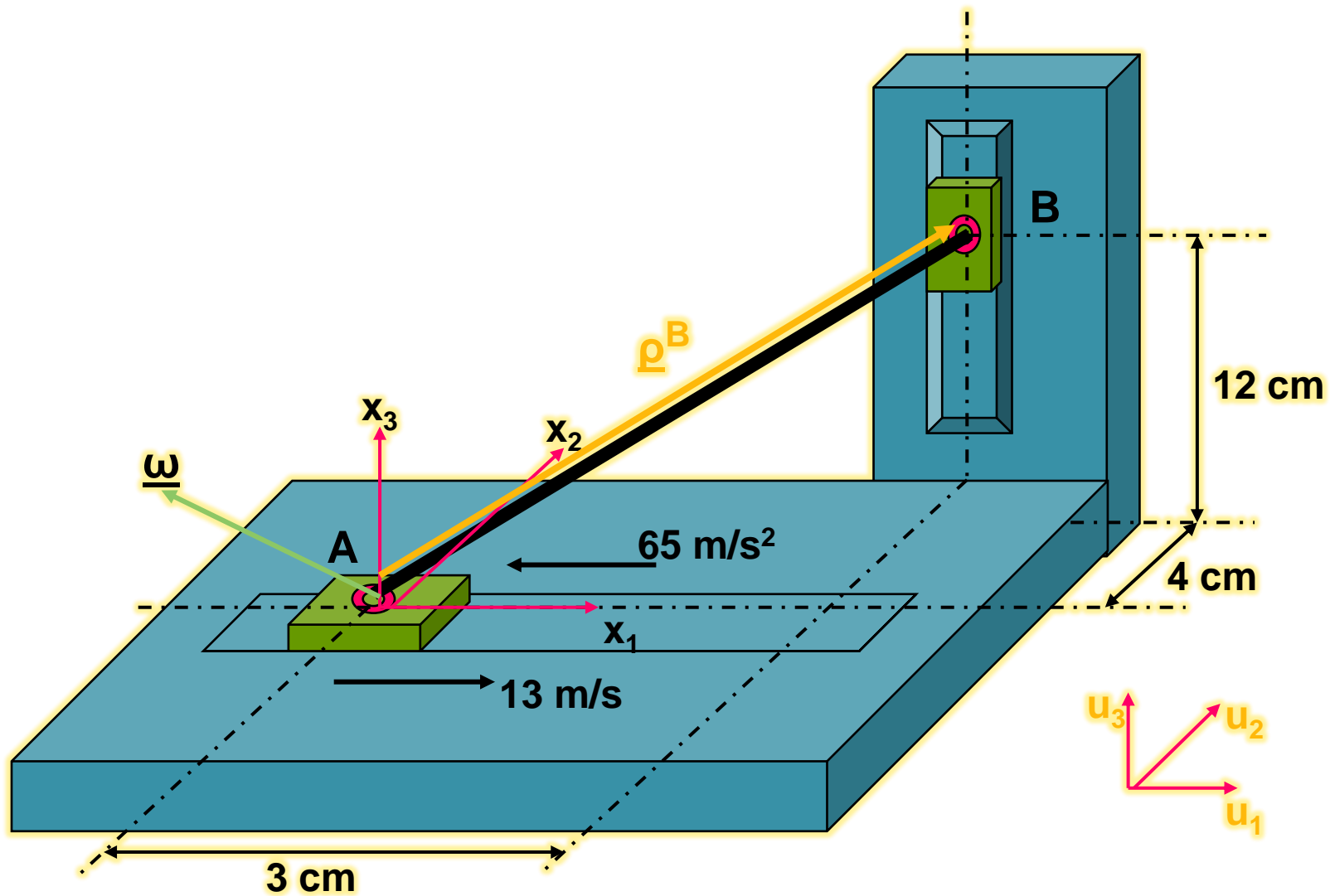
Solution:

Consider the rigid body **AB**, where:

A: is the reference body point, and

B: is the body point whose motion is to be analyzed.





Step-1: Motion (pos., vel., acc.) of point “B”;

$$\underline{\rho}^B = 3\underline{u}_1 + 4\underline{u}_2 + 12\underline{u}_3$$

$$\underline{v}_B = v_B \underline{u}_3, \quad \text{and} \quad \underline{a}_B^{\text{cm}} = a_B \underline{u}_3$$

Step-2: Motion of reference point “A”;

$$\underline{v}_A = 1300\underline{u}_1 \text{ cm/s}, \quad \text{and} \quad \underline{a}_A = -6500\underline{u}_1 \text{ cm/s}^2$$

Step-3: The angular motions of AB is unknown. Since the axial component of the angular motions of AB do not contribute to the motion of point “B”, we impose the following conditions;

$$\left\{ \begin{array}{l} \underline{\omega} \cdot \underline{e}_{B/A} = \underline{\omega} \cdot \frac{\underline{\rho}^B}{|\underline{\rho}^B|} = 0 \\ \underline{\alpha} \cdot \underline{e}_{B/A} = \underline{\alpha} \cdot \frac{\underline{\rho}^B}{|\underline{\rho}^B|} = 0 \end{array} \right\} \Rightarrow \left\{ \begin{array}{l} \underline{\omega} \cdot \underline{\rho}^B = 3\omega_1 + 4\omega_2 + 12\omega_3 = 0 \quad (a) \\ \underline{\alpha} \cdot \underline{\rho}^B = 3\alpha_1 + 4\alpha_2 + 12\alpha_3 = 0 \quad (b) \end{array} \right\}$$



Step-4: Velocity Analysis;

$$\underline{v}_B = \underline{v}_A + \underline{\omega} \times \underline{\rho}^B$$

$$v_B \underline{u}_3 = 1300 \underline{u}_1 + (\omega_1 \underline{u}_1 + \omega_2 \underline{u}_2 + \omega_3 \underline{u}_3) \times (3 \underline{u}_1 + 4 \underline{u}_2 + 12 \underline{u}_3)$$

$$\left\{ \begin{array}{ll} \underline{u}_1 : & 0 = 1300 + 12\omega_2 - 4\omega_3 \quad (c) \\ \underline{u}_2 : & 0 = 3\omega_3 - 12\omega_1 \quad (d) \\ \underline{u}_3 : & v_B = 4\omega_1 - 3\omega_2 \quad (e) \end{array} \right\}$$

From expressions (a, c, d, e), we have:

$$\underline{v}_B = 325 \underline{u}_3 \text{ cm/s, and } \underline{\omega} = (100 \underline{u}_1 - 1275 \underline{u}_2 + 400 \underline{u}_3) / 13 \text{ rad/s}$$



Step-5: Acceleration Analysis;

$$\underline{a}_B = \underline{a}_A + \underline{\alpha} \times \underline{\rho}^B + \underline{\omega} \times (\underline{\omega} \times \underline{\rho}^B) \quad \Rightarrow$$

$$\left\{ \begin{array}{ll} \underline{u}_1 : & 0 = -6500 + 12\alpha_2 - 4\alpha_3 - 31875 \quad (f) \\ \underline{u}_2 : & 0 = 3\alpha_3 - 12\alpha_1 - 42500 \quad (g) \\ \underline{u}_3 : & a_B = 4\alpha_1 - 3\alpha_2 - 127500 \quad (h) \end{array} \right\}$$

From expressions (b, f, g, h) , we have:

$$\underline{a}_B = -151260\underline{u}_3 \text{ cm/s}^2, \quad \text{and} \quad \underline{\alpha} = -3580\underline{u}_1 + 3146.6\underline{u}_2 - 153.8\underline{u}_3 \text{ rad/s}^2$$

Also: $x_1^2 + x_2^2 + x_3^2 = \ell^2 = \text{const}$

$$\frac{d}{dt}(\dots) = 2\dot{x}_1 x_1 + 2\dot{x}_2 x_2 + 2\dot{x}_3 x_3 = 0 \quad \Rightarrow \quad \dot{x}_3 = ?$$

$$\frac{d}{dt}(\dots) = \ddot{x}_1 x_1 + \dot{x}_1^2 + \ddot{x}_3 x_3 + \dot{x}_3^2 = 0 \quad \Rightarrow \quad \ddot{x}_3 = ?$$



مختصر