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INERTIA TENSOR

Purpose:

- To Study Inertia Tensor of a Material System.

Topics:

- Inertia Tensor of a Mass Particle.
- Inertia Tensor of a System of Particles.
- Inertia Tensor of a Continuum.
- Transfer Theorem.
- Principal Values of Inertia Tensor.



From **Chapter-6**, we defined the **Kinetic States** as:

❖ **For a Single particle;**

Linear Momentum (Momentum):

$$\underline{P} = m\underline{v} \quad \text{or} \quad P_i = mv_i \quad (7.1)$$

Moment of Momentum (Angular Momentum):

$$\underline{H}^O = \underline{r} \times \underline{P} = m\underline{r} \times \underline{\dot{r}}, \quad \text{or} \quad (7.2)$$

$$H_i^O = \gamma_{ijk} x_j P_k, \text{ where: "O" is a moment center.}$$



❖ For a System of Particles;

Linear Momentum (Momentum):

$$\underline{P} = \sum_{\beta=1}^N \underline{P}^{\beta} = \sum_{\beta=1}^N m_{\beta} \underline{v}^{\beta}, \quad \text{or} \quad (7.3)$$

$$P_i = \sum_{\beta=1}^N P_i^{\beta} \quad (i = 1, 2, 3)$$

Moment of Momentum (Angular Momentum):

$$\underline{H}^O = \sum_{\beta=1}^N \underline{H}_{\beta}^O = \sum_{\beta=1}^N \underline{r}^{\beta} \times \underline{P}^{\beta} = \sum_{\beta=1}^N m_{\beta} \underline{r}^{\beta} \times \underline{v}^{\beta}, \quad \text{or} \quad (7.4)$$

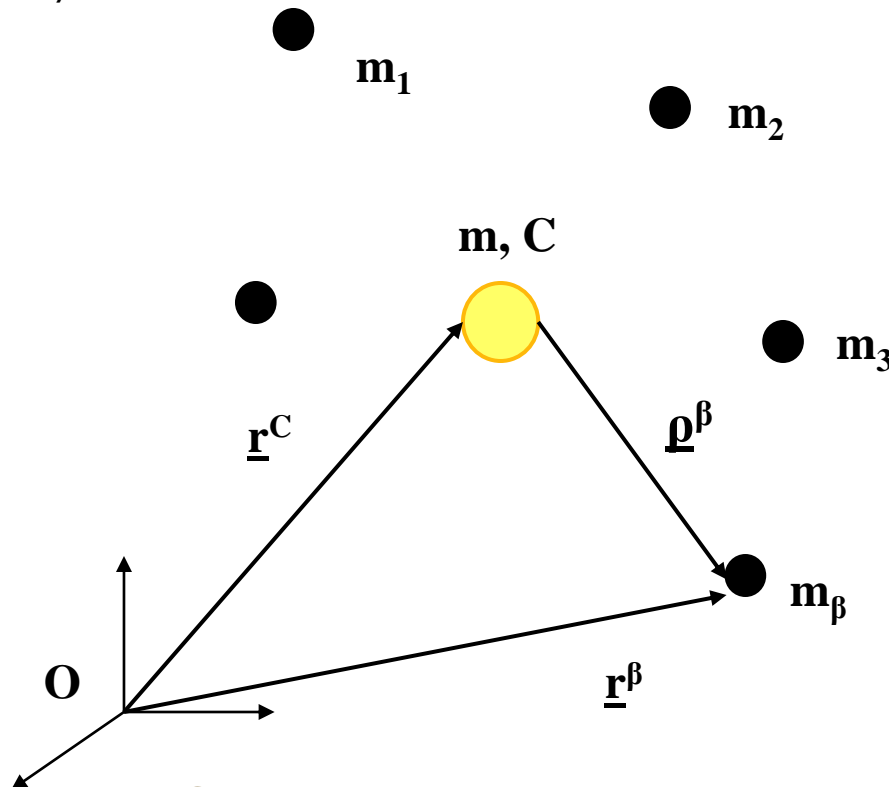
$$H_i^{\beta} = \sum_{\beta=1}^N \gamma_{ijk} x_j^{\beta} P_k^{\beta} \quad (i, j, k \equiv 1, 2, 3)$$

Where; \underline{r}^{β} : position vector of the “ β th” particle from the moment center “O”.



or, by **Theorem-16**, for the equivalent mass system, the Total/Global Momentum and Global Moment of Momentum of the system of particles is:

$$\underline{P} = m \underline{v}^C = \sum_{\beta=1}^N m_{\beta} \underline{v}^{\beta} = \text{(\underline{Global Momentum})} \quad (7.5)$$

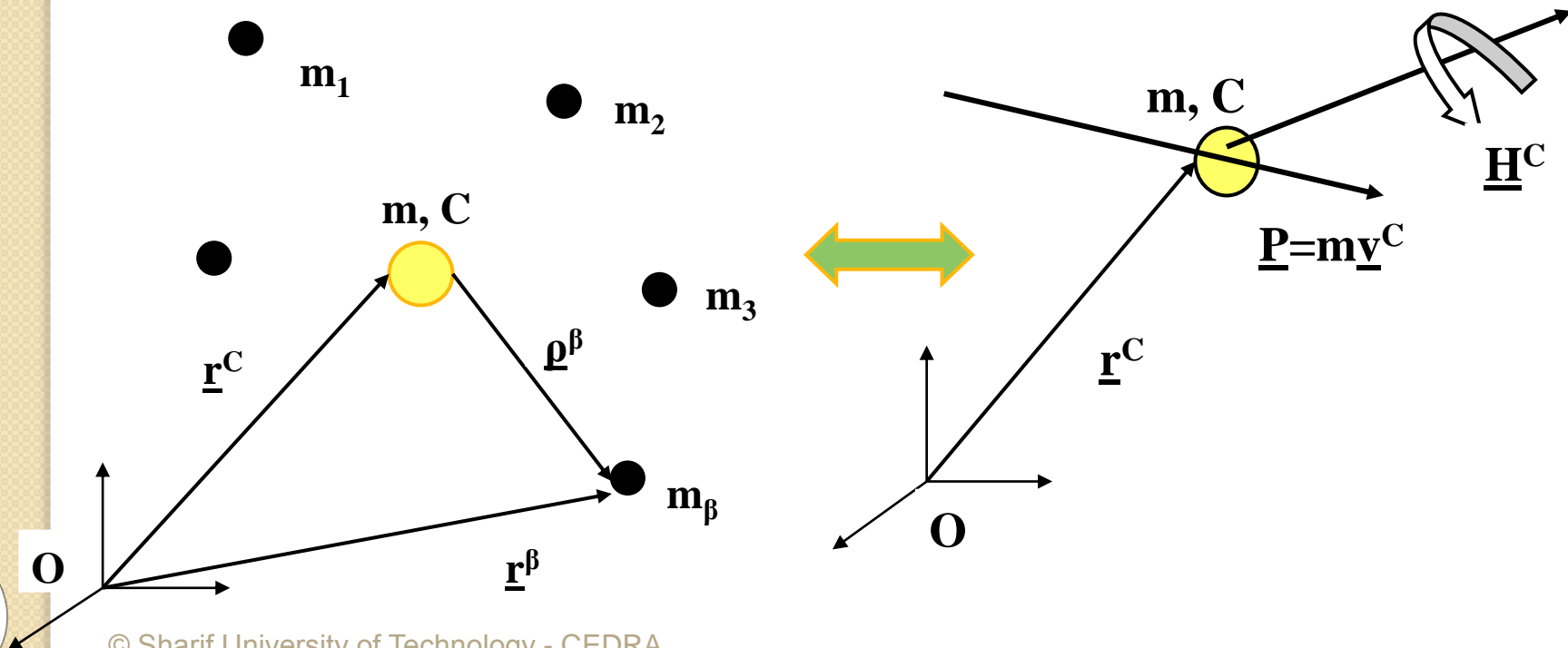


$$\underline{H}^O = \underline{H}^C + \underline{r}^C \times \underline{P} = \underline{H}^C + \underline{H}_{eq}^O \quad (\text{Global M.O.M.}) \quad (7.6)$$

Where; \underline{H}^O : (M.O.M. about any point "O" in space).

$$\underline{H}^C = \sum_{\beta=1}^N \underline{\rho}^{\beta} \times \underline{P}^{\beta} = \sum_{\beta=1}^N \underline{\rho}^{\beta} \times m_{\beta} \underline{\dot{\rho}}^{\beta} \quad (\text{Central M.O.M.})$$

$$\underline{H}_{eq}^O = \underline{r}^C \times \underline{P}$$



Now, let us consider the system of particles shown.

We wish to define the quantity $\underline{H}^C = ?$ (Central M.O.M.).

To do this, suppose that the system is:

- Locked rigidly, so that the distance between any pair of particles remain constant throughout the dynamic process.

Therefore: The system's rotation may be described by a single angular velocity " $\underline{\omega}$ ".

$$\underline{H}^C = \sum_{\beta=1}^N \underline{\rho}^{\beta} \times \underline{P}^{\beta} = \sum_{\beta=1}^N \underline{\rho}^{\beta} \times m_{\beta} \underline{\dot{\rho}}^{\beta} \quad \text{where : } \left\{ \begin{array}{l} |\underline{\rho}| \equiv \text{const.} \\ \{m_{\beta}\} \equiv \text{rigid} \\ C \equiv \text{Body - Point} \end{array} \right\}$$



$\underline{\rho}^\beta = \bar{x}_i^\beta \underline{u}_i$; where $\{\bar{x}_i\}$: its origin is at the mass center.

$$\underline{\omega}_\beta = \underline{\omega}$$

Therefore:
$$\dot{\underline{\rho}}^\beta = \underline{\omega} \times \underline{\rho}^\beta$$

Hence:

$$\underline{H}^C = \sum_{\beta=1}^N m_\beta \underline{\rho}^\beta \times (\underline{\omega} \times \underline{\rho}^\beta) \quad \text{or} \quad H_i^C = \left[\sum_{\beta=1}^N m_\beta \underline{\rho}^\beta \times (\underline{\omega} \times \underline{\rho}^\beta) \right]_i$$

But,

$$\underline{\rho}^\beta \times (\underline{\omega} \times \underline{\rho}^\beta) = (\underline{\rho}^\beta \cdot \underline{\rho}^\beta) \underline{\omega} - (\underline{\rho}^\beta \cdot \underline{\omega}) \underline{\rho}^\beta$$



$$\begin{aligned}
 [\underline{\rho}^\beta \times (\underline{\omega} \times \underline{\rho}^\beta)]_i &= (\underline{\rho}^\beta \cdot \underline{\rho}^\beta) \omega_i - (\underline{\rho}^\beta \cdot \underline{\omega}) \bar{x}_i^\beta \\
 &= (\bar{x}_k^\beta \bar{x}_k^\beta) \omega_j \delta_{ij} - (\bar{x}_j^\beta \omega_j) \bar{x}_i^\beta \\
 &= (\bar{x}_k^\beta \bar{x}_k^\beta \delta_{ij} - \bar{x}_i^\beta \bar{x}_j^\beta) \omega_j
 \end{aligned}$$

Therefore:

$$\begin{aligned}
 H_i^C &= \left[\sum_{\beta=1}^N m_\beta (\bar{x}_k^\beta \bar{x}_k^\beta \delta_{ij} - \bar{x}_i^\beta \bar{x}_j^\beta) \right] \omega_j \\
 &= I_{ij}^C \omega_j
 \end{aligned} \tag{7.7}$$

$$\underline{H}^C = \underline{\underline{I}}^C \cdot \underline{\omega}$$

where:



$$\underline{\underline{I}}^C \equiv I_{ij}^C = \left[\sum_{\beta=1}^N m_{\beta} (\bar{x}_k^{\beta} \bar{x}_k^{\beta} \delta_{ij} - \bar{x}_i^{\beta} \bar{x}_j^{\beta}) \right] \quad (7.8)$$

\equiv (***The Inertia Tensor***; a 2nd order and symmetrical tensor), or:

$$I_{ij}^C \equiv \begin{bmatrix} I_{11}^C & I_{12}^C & I_{13}^C \\ I_{21}^C & I_{22}^C & I_{23}^C \\ I_{31}^C & I_{32}^C & I_{33}^C \end{bmatrix}$$

Compare (for a rigid system): $\left\{ \begin{array}{l} \underline{H}^C = \underline{\underline{I}}^C \cdot \underline{\omega} \\ \underline{P} = m \underline{v}^C \end{array} \right\}$ **where:**

$\underline{\omega}$ and \underline{v}^C : are the velocity properties, and

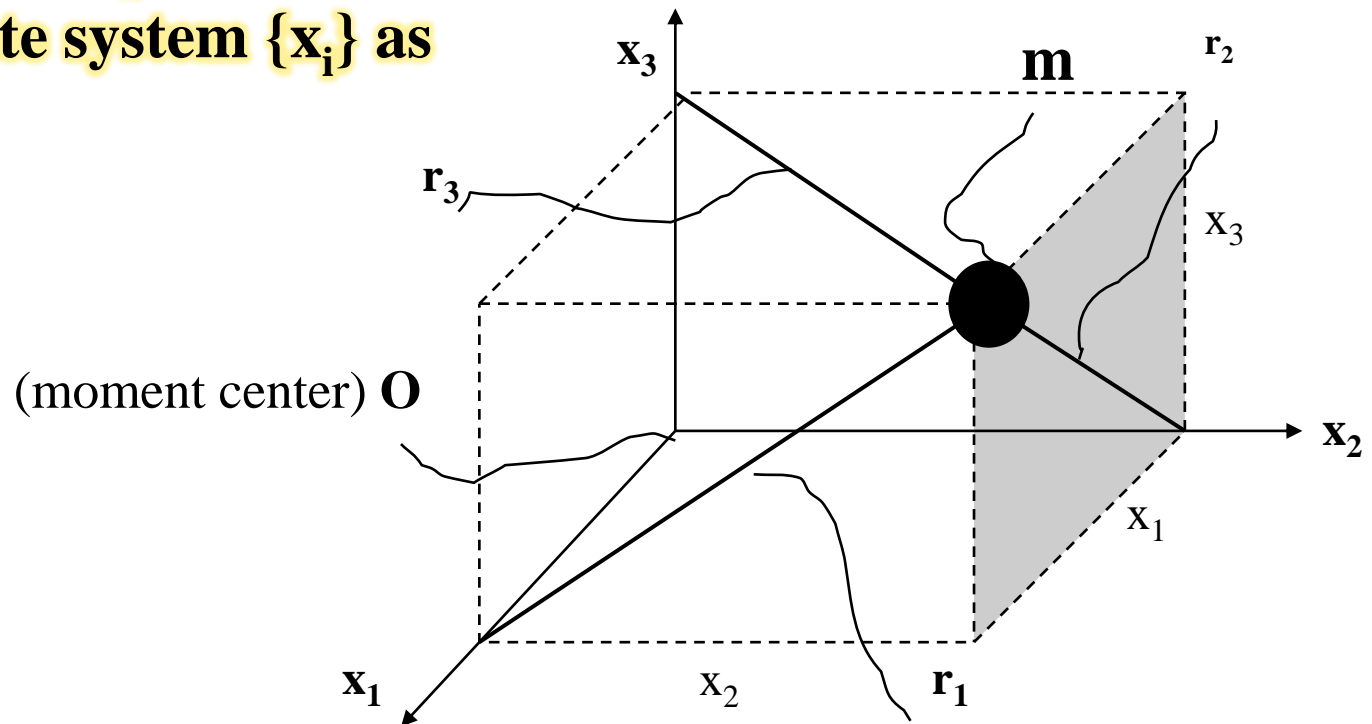
$\underline{\underline{I}}^C$: plays the role of mass “m” in describing the kinetic state of a rigid system.



Definition: The “Inertia Tensor” actually defines the mass distribution of a material system.

Inertia Tensor of a Particle of Mass “m” about a fixed point “O”:

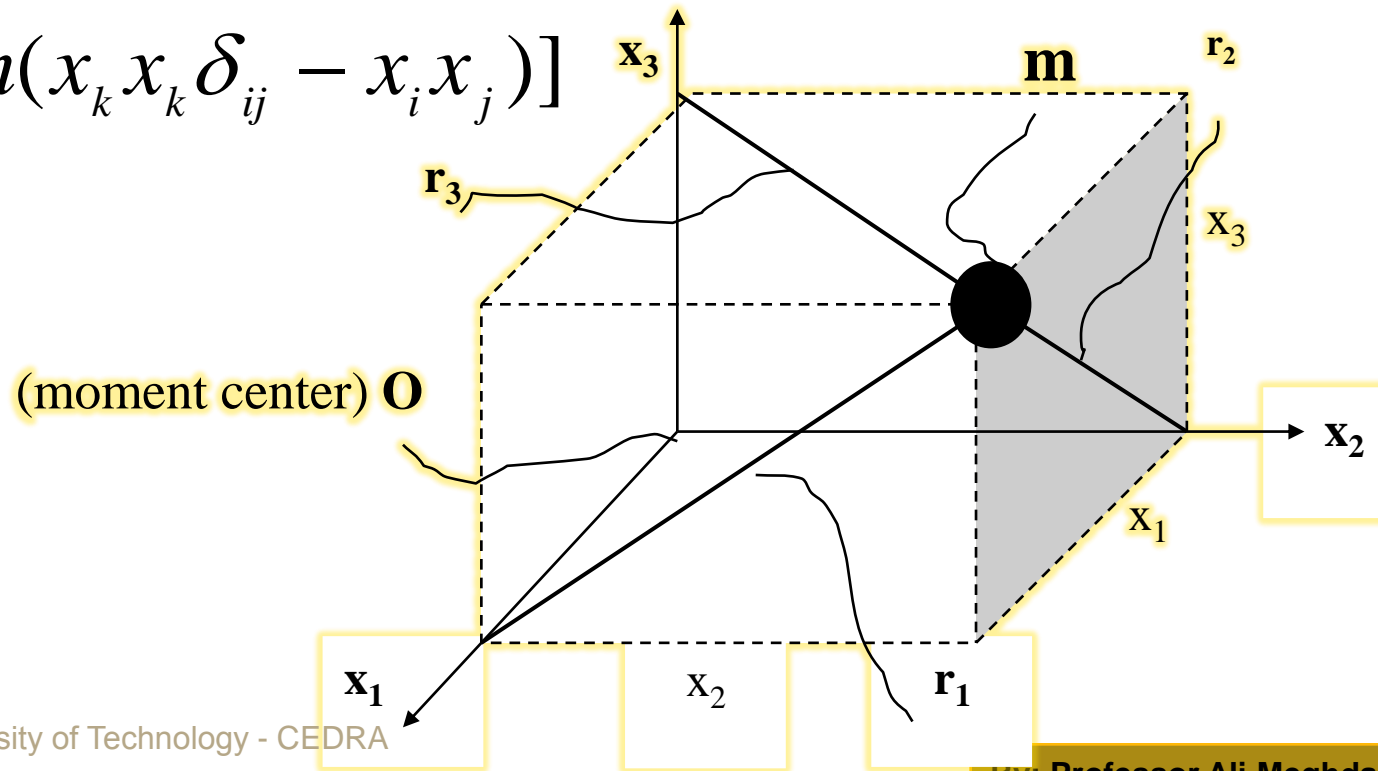
Consider the particle “m” in coordinate system $\{x_i\}$ as shown;



$$\begin{aligned}
 \underline{H}^O &= \underline{r} \times \underline{P} = \underline{r} \times m \underline{v} = \underline{r} \times m \underline{\dot{r}} \\
 &= m \underline{r} \times (\underline{\omega} \times \underline{r}) \\
 &= m(\underline{r} \cdot \underline{r})\underline{\omega} - (\underline{r} \cdot \underline{\omega})\underline{r}
 \end{aligned}$$

$$H_i^O = [m(x_k x_k \delta_{ij} - x_i x_j)] \omega_j \quad (7.9)$$

$$I_{ij}^O = [m(x_k x_k \delta_{ij} - x_i x_j)]$$



$$I_{ij}^O = [m(x_k x_k \delta_{ij} - x_i x_j)] \quad (7.9)$$

Definition: The moments of inertia of the particle “m” about the axes $\{x_i\}$ are:

$$\begin{aligned} I_{11}^O &= m(x_1^2 + x_2^2 + x_3^2 - x_1^2) = m(x_2^2 + x_3^2) = mr_1^2 & \text{for } i=1, j=1 \\ I_{22}^O &= m(x_1^2 + x_2^2 + x_3^2 - x_2^2) = m(x_1^2 + x_3^2) = mr_2^2 & \text{for } i=2, j=2 \\ I_{33}^O &= m(x_1^2 + x_2^2 + x_3^2 - x_3^2) = m(x_1^2 + x_2^2) = mr_3^2 & \text{for } i=3, j=3 \end{aligned}$$

Definition: The products of inertia of the particle “m” are:

$$\begin{aligned} I_{12}^O &= m(0 - x_1 x_2) = -mx_1 x_2 & \text{for } i=1, j=2 \\ I_{23}^O &= m(0 - x_2 x_3) = -mx_2 x_3 & \text{for } i=2, j=3 \\ I_{31}^O &= m(0 - x_3 x_1) = -mx_3 x_1 & \text{for } i=3, j=1 \end{aligned}$$



Inertia Tensor of a System of Particles about a fixed point “O”: A physical property of the material system;

$$I_{ij}^O = \sum_{\beta=1}^N m_{\beta} [x_k^{\beta} x_k^{\beta} \delta_{ij} - x_i^{\beta} x_j^{\beta}] \quad (7.10)$$

$$I_{ij}^O = \sum_{\beta=1}^N m_{\beta} \begin{bmatrix} (x_2^{\beta})^2 + (x_3^{\beta})^2 & -x_1^{\beta} x_2^{\beta} & -x_1^{\beta} x_3^{\beta} \\ -x_2^{\beta} x_1^{\beta} & (x_3^{\beta})^2 + (x_1^{\beta})^2 & -x_2^{\beta} x_3^{\beta} \\ -x_3^{\beta} x_1^{\beta} & -x_3^{\beta} x_2^{\beta} & (x_1^{\beta})^2 + (x_2^{\beta})^2 \end{bmatrix}$$

Note: To write the inertia tensor about an arbitrary point “A” in space, simply do a **coordinate shift**, as:

$$I_{ij}^A = \sum_{\beta=1}^N m_{\beta} [(x_k^{\beta} - x_k^A)(x_k^{\beta} - x_k^A) \delta_{ij} - (x_i^{\beta} - x_i^A)(x_j^{\beta} - x_j^A)] \quad (7.11)$$

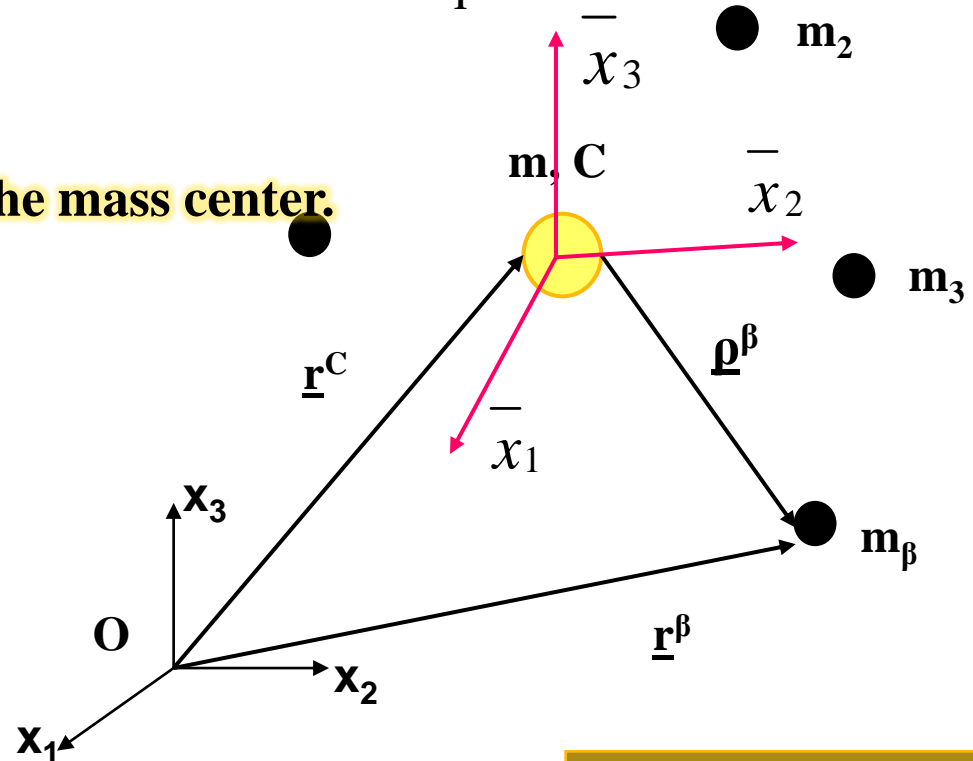


Definition: When the moment center is specifically the mass center, the inertia tensor is called the **Central Inertia Tensor**, “ $\underline{\underline{I}}^C$ ”, where:

$$I_{ij}^C = \sum_{\beta=1}^N m_{\beta} [\bar{x}_k^{\beta} \bar{x}_k^{\beta} \delta_{ij} - \bar{x}_i^{\beta} \bar{x}_j^{\beta}] ; \quad (7.12)$$

Where:

$\{\bar{x}_i\}$: its origin is located at the mass center.



Inertia Tensor for a Continuum: A generalization of the inertia tensor for a system of particles where the finite sums “ \sum ” are integrally summed “ \int ”.

$$I_{ij}^O = \int_m (x_k x_k \delta_{ij} - x_i x_j) dm \quad (7.13)$$

Ex:
$$\left\{ \begin{array}{l} I_{11}^O = \int_m (x_2^2 + x_3^2) dm \\ I_{12}^O = - \int_m x_1 x_2 dm \end{array} \right\}$$

And about any **arbitrary moment center** like “A” is:

$$I_{ij}^A = \int_m [(x_k - x_k^A)(x_k - x_k^A) \delta_{ij} - (x_i - x_i^A)(x_j - x_j^A)] dm \quad (7.14)$$



Transfer Theorem-(18): When the mass, the mass center, and the central inertia tensor are known, the inertia tensor of a mass system about any given moment center can be obtained from:

$$I_{ij}^A = m[(x_k^C - x_k^A)(x_k^C - x_k^A)\delta_{ij} - (x_i^C - x_i^A)(x_j^C - x_j^A)] + I_{ij}^C$$
$$\underline{I}^A = \underline{I}_{eq.}^A + \underline{I}^C \quad (7.15)$$

where; $\underline{I}_{eq.}^A$: inertia tensor about “A” due to a single particle of mass “m” at the mass center.



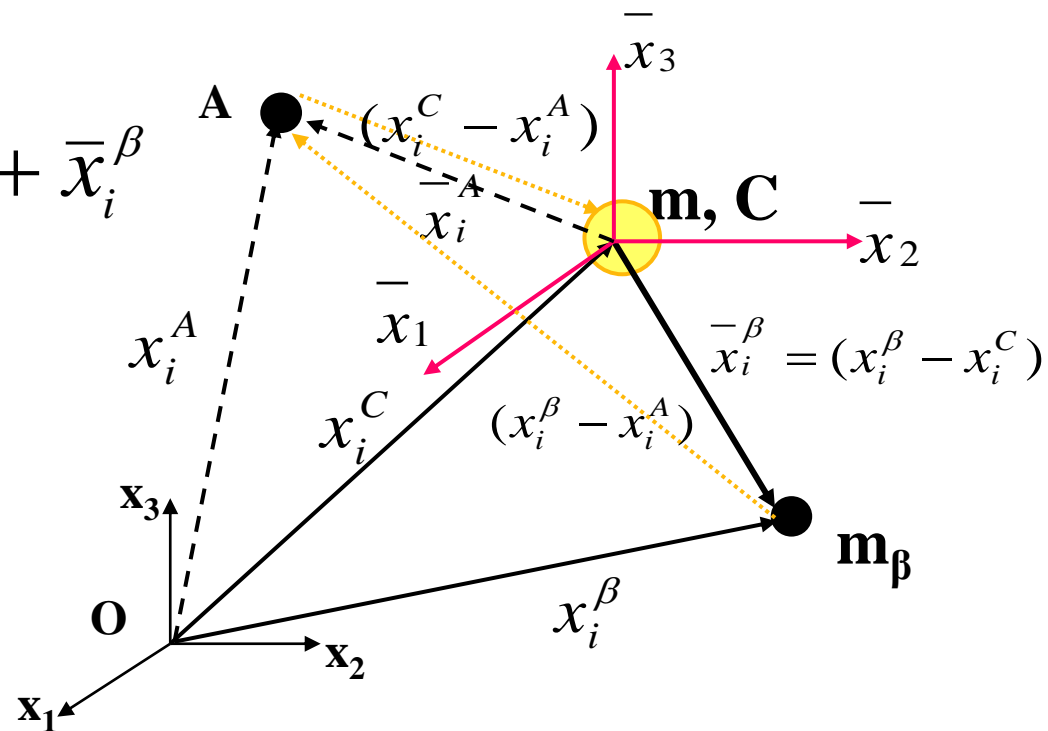
Proof:

$\{\bar{x}_i\}$: its origin is located at the mass center.

$\{x_i\}$: its origin is located at the fixed point “O”.

$$x_i^\beta = x_i^C + \bar{x}_i^\beta$$

$$x_i^\beta - x_i^A = x_i^C - x_i^A + \bar{x}_i^\beta$$



$$(x_i^\beta - x_i^A) = (x_i^C - x_i^A) + (x_i^\beta - x_i^C)$$

$$(x_i^\beta - x_i^A) = (x_i^C - x_i^A) + (x_i^\beta - x_i^C)$$

Substituting the last equation into the Equation (7.11) and simplifying results in:

Note: *Inertia Tensor* about an arbitrary point “A” in space, can be computed by a coordinate shift, as:

$$I_{ij}^A = \sum_{\beta=1}^N m_\beta [(x_k^\beta - x_k^A)(x_k^\beta - x_k^A)\delta_{ij} - (x_i^\beta - x_i^A)(x_j^\beta - x_j^A)] \quad (7.11)$$

$$I_{ij}^A = m[(x_k^C - x_k^A)(x_k^C - x_k^A)\delta_{ij} - (x_i^C - x_i^A)(x_j^C - x_j^A)] + I_{ij}^C \quad (7.15)$$

However, if the origin “O” is selected as the moment center, then $x_i^A = 0$, and Equation (7.15) reduces to:



$$\left\{ \begin{aligned} I_{ij}^O &= m(x_k^C x_k^C \delta_{ij} - x_i^C x_j^C) + I_{ij}^C \\ \underline{\underline{I}}^O &= \underline{\underline{I}}_{eq.}^O + \underline{\underline{I}}^C \end{aligned} \right. \quad (7.16)$$

or:

$$\underline{\underline{I}}^O = \underline{\underline{I}}^C + m \begin{bmatrix} (x_2^C)^2 + (x_3^C)^2 & -x_1^C x_2^C & -x_1^C x_3^C \\ -x_2^C x_1^C & (x_3^C)^2 + (x_1^C)^2 & -x_2^C x_3^C \\ -x_3^C x_1^C & -x_3^C x_2^C & (x_1^C)^2 + (x_2^C)^2 \end{bmatrix}$$

(7.17)



Principal Values of the Inertia Tensor: In rigid body dynamics, it is often convenient to use a coordinate system fixed to the rigid body in which the products of inertia are zero. In this case, the inertia tensor “ \underline{I} ” will be a diagonal matrix such as:

$$I_{\alpha} = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \quad (7.18)$$

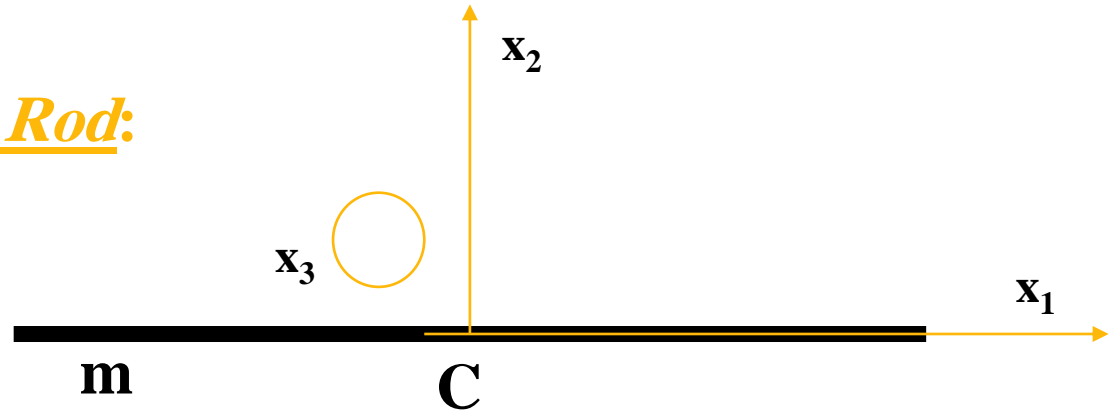
This coordinate system is then called the Principal Coordinate, and the moments of inertia about the principal axes are called the Principal Moments of Inertia, and the three planes formed by the principal axes are called the Principal Planes.



Example:

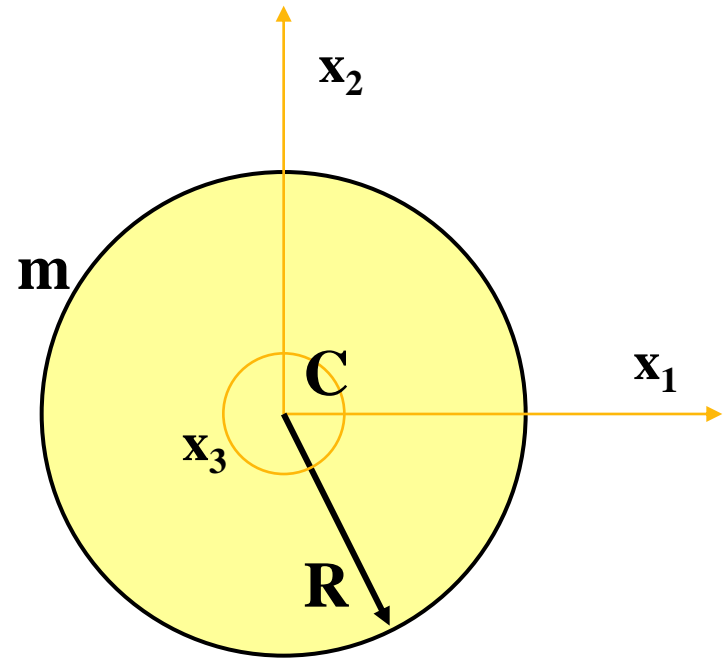
➤ A Thin Uniform Rod:

$$\underline{\underline{I}}^C = \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{ml^2}{12} & 0 \\ 0 & 0 & \frac{ml^2}{12} \end{bmatrix}$$



➤ A Thin Uniform Disk:

$$\underline{\underline{I}}^C = \begin{bmatrix} \frac{1}{4}mR^2 & 0 & 0 \\ 0 & \frac{1}{4}mR^2 & 0 \\ 0 & 0 & \frac{1}{2}mR^2 \end{bmatrix}$$



➤ *A Sphere of Radius “R” and Mass “m”:*

$$\underline{\underline{I}}^c = \frac{2}{5}mR^2 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

More on the Principal Inertia Tensor: If we examine the moment and product of inertia terms for all possible orientation of the coordinate axes with respect to a rigid body for a given origin, we will find in the general case *one unique orientation* “ $\{\mathbf{x}_a\}$ ” for which the products of inertia are zero.



Theorem-19: Given “ $\underline{\underline{I}}^O = I_{ij}^O$ ”, there exist three principal values of “ $\underline{\underline{I}}^O$ ”, namely I_{α}^O (Principal Moments of Inertia) which are the eigenvalues of the inertia tensor I_{ij}^O , and may be computed as follows:

$$\left| I_{ij}^O - I_{\alpha}^O \underline{\underline{E}} \right| = 0, \text{ and let } I_{\alpha}^O \equiv I(\underline{\underline{E}} = \underline{\underline{Unit Matrix}} = \delta_{ij})$$

therefore;

(7.19)

$$I^3 - J_1 I^2 - J_2 I - J_3 = 0 \quad (\text{Characteristic - Equation}), \quad \text{where :}$$

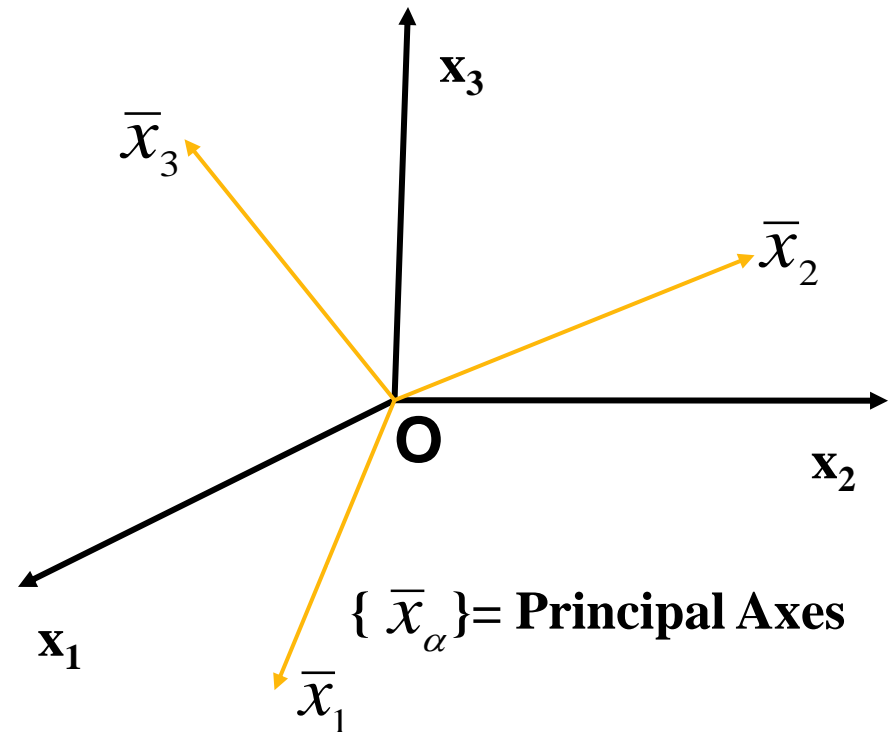
$$J_1 = I_{ii}^O$$

$$J_2 = \frac{1}{2} (I_{ij}^O I_{ij}^O - I_{ii}^O I_{jj}^O) \quad (7.20)$$

$$J_3 = \left| I_{ij}^O \right|$$



and the **direction cosines of the principal axes of inertia** $\{\ell_{i\alpha}\}$ are the corresponding **normalized eigenvectors**, defined as follows:



$$(I_{ij}^O - I_\alpha^O \delta_{ij}) \ell_{i\alpha} = 0$$

$$\ell_{i\alpha} \ell_{i\alpha} = 1$$

(7.21)



Example: For the \bar{x}_1 - axis we can write:

$$\left\{ \begin{array}{l} (I_{11}^O - I_1^O)\ell_{1\bar{1}} + I_{21}^O\ell_{2\bar{1}} + I_{31}^O\ell_{3\bar{1}} = 0 \\ I_{12}^O\ell_{1\bar{1}} + (I_{22}^O - I_1^O)\ell_{2\bar{1}} + I_{32}^O\ell_{3\bar{1}} = 0 \\ I_{13}^O\ell_{1\bar{1}} + I_{23}^O\ell_{2\bar{1}} + (I_{33}^O - I_1^O)\ell_{3\bar{1}} = 0 \\ \ell_{1\bar{1}}^2 + \ell_{2\bar{1}}^2 + \ell_{3\bar{1}}^2 = 1 \end{array} \right. \quad (7.22)$$

From equations (7.22), we can write:

$$\bar{e}_1 \equiv \left\{ \begin{array}{l} \ell_{1\bar{1}} \underline{e}_1 \\ \ell_{2\bar{1}} \underline{e}_2 \\ \ell_{3\bar{1}} \underline{e}_3 \end{array} \right\}$$

(In the first 3 Equations of (7.22), only 2 are independent, and the 3rd is a linear combination of the others.)



And similarly for \bar{x}_2 and \bar{x}_3 axes we have:

$$\bar{e}_2 \equiv \begin{Bmatrix} l_{1\bar{2}} \underline{e}_1 \\ l_{2\bar{2}} \underline{e}_2 \\ l_{3\bar{2}} \underline{e}_3 \end{Bmatrix}, \quad \bar{e}_3 \equiv \begin{Bmatrix} l_{1\bar{3}} \underline{e}_1 \\ l_{2\bar{3}} \underline{e}_2 \\ l_{3\bar{3}} \underline{e}_3 \end{Bmatrix}, \text{ and therefore:}$$

$$\{\bar{e}_\alpha\} \equiv \begin{bmatrix} l_{1\bar{1}} & l_{2\bar{1}} & l_{3\bar{1}} \\ l_{1\bar{2}} & l_{2\bar{2}} & l_{3\bar{2}} \\ l_{1\bar{3}} & l_{2\bar{3}} & l_{3\bar{3}} \end{bmatrix} \{\underline{e}_i\} \equiv \underline{\underline{T}} \{\underline{e}_i\}, \quad \text{or} \quad (7.23)$$

$$\{\underline{e}_i\} \equiv \begin{bmatrix} l_{1\bar{1}} & l_{1\bar{2}} & l_{1\bar{3}} \\ l_{2\bar{1}} & l_{2\bar{2}} & l_{2\bar{3}} \\ l_{3\bar{1}} & l_{3\bar{2}} & l_{3\bar{3}} \end{bmatrix} \{\bar{e}_\alpha\} \equiv \underline{\underline{T}}^t \{\bar{e}_\alpha\}$$



Now, let us consider the **Moment of Momentum** vector about the point “O”, such that:

$$\{\underline{H}^O\}_\alpha = [\underline{T}]\{\underline{H}^O\}_i \quad (7.24)$$

But:
$$\begin{cases} \{\underline{H}^O\}_\alpha = [I_\alpha^O]\{\underline{\omega}\}_\alpha \\ \{\underline{H}^O\}_i = [I_{ij}^O]\{\underline{\omega}\}_i \end{cases}$$

substituting in equation (7.24) results:

$$\begin{aligned} [I_\alpha^O]\{\underline{\omega}\}_\alpha &= [\underline{T}][I_{ij}^O]\{\underline{\omega}\}_i \\ &= \{ [\underline{T}][I_{ij}^O][\underline{T}^t] \} \{ [\underline{T}]\{\underline{\omega}\}_i \} \\ &= \{ [\underline{T}][I_{ij}^O][\underline{T}^t] \} \{\underline{\omega}\}_\alpha \end{aligned}$$



$$\begin{aligned}
 \underbrace{[I_{\alpha}^O]} \{\underline{\omega}\}_{\alpha} &= [\underline{T}][I_{ij}^O] \{\underline{\omega}\}_i \\
 &= \{ [\underline{T}][I_{ij}^O][\underline{T}^t] \} \{ [\underline{T}]\{\underline{\omega}\}_i \} \\
 &= \underbrace{\{ [\underline{T}][I_{ij}^O][\underline{T}^t] \}} \{\underline{\omega}\}_{\alpha}
 \end{aligned}$$

Therefore:

$$[I_{\alpha}^O] = [\underline{T}][I_{ij}^O][\underline{T}^t] \quad (7.25)$$

Equation (7.25) is known as the Rotation Transformation of Inertia Properties. (same as Eq. 5.54 in Ginsberg Book)



Theorem-20: For a body with a plane of symmetry, any axis perpendicular to the plane is a principal axis of inertia at the point of intersection with that plane. (*In other words, if two coordinate axes form a plane of symmetry for a body, then all product of inertias involving the coordinate normal to that plane are zero*).

Theorem-21: For a body having two planes of symmetry, the line of intersection is also the principal axis for any moment center lying on the line.

Theorem-22: If at least two of the three coordinate planes are planes of symmetry for a body, then all products of inertias are zero.



مختصر

For a Matrix $\underline{\underline{A}}$:

Eigenvalues: $\left| \underline{\underline{A}} - \lambda \underline{\underline{I}} \right| = 0$, ($\underline{\underline{I}} = \underline{\underline{Unit Matrix}} = \delta_{ij}$)

Eigenvectors:

$$\left| \underline{\underline{A}} - \lambda \underline{\underline{I}} \right| \{ \underline{x} \} = \{ \underline{0} \}, (\underline{\underline{I}} = \underline{\underline{Unit Matrix}} = \delta_{ij})$$

(READ EXAMPLES 5.1 and 5.3 of Ginsburg)

